

Exercise 4.1

Displacement formulation of linear elastodynamics: strong and weak forms, Galerkin FE model

General IVP of linear elastodynamics

Find $u_i = u_i(\mathbf{x}, t) = ?$, $\varepsilon_{ij} = \varepsilon_{ij}(\mathbf{x}, t) = ?$, $\sigma_{ij} = \sigma_{ij}(\mathbf{x}, t) = ?$ satisfying in Ω :

$$\sigma_{ij|j} + f_i = \varrho \ddot{u}_i, \quad \varepsilon_{ij} = \frac{1}{2}(u_{i|j} + u_{j|i}), \quad \sigma_{ij} = \begin{cases} C_{ijkl} \varepsilon_{kl} & \text{(anisotropy),} \\ 2\mu \varepsilon_{ij} + \lambda \varepsilon_{kk} \delta_{ij} & \text{(isotropy),} \end{cases}$$

with the initial conditions (at $t = t_0$):

$$u_i(\mathbf{x}, t_0) = u_i^0(\mathbf{x}) \quad \text{and} \quad \dot{u}_i(\mathbf{x}, t_0) = v_i^0(\mathbf{x}) \quad \text{in } \Omega,$$

and subject to the boundary conditions on $\Gamma = \Gamma_u \cup \Gamma_t$ ($\Gamma_u \cap \Gamma_t = \emptyset$):

$$u_i(\mathbf{x}, t) = \hat{u}_i(\mathbf{x}, t) \quad \text{on } \Gamma_u, \quad \sigma_{ij}(\mathbf{x}, t) n_j = \hat{t}_i(\mathbf{x}, t) \quad \text{on } \Gamma_t.$$

1. Derive the displacement formulation of elasticity (Navier's equations)
2. Derive the weak variational form of the displacement formulation
3. Derive the Galerkin FE model (i.e., $\mathbf{M} \ddot{\mathbf{q}}(t) + \mathbf{K} \mathbf{q}(t) = \mathbf{Q}(t)$)

Exercise 4.2

A simple thermo-elastic problem

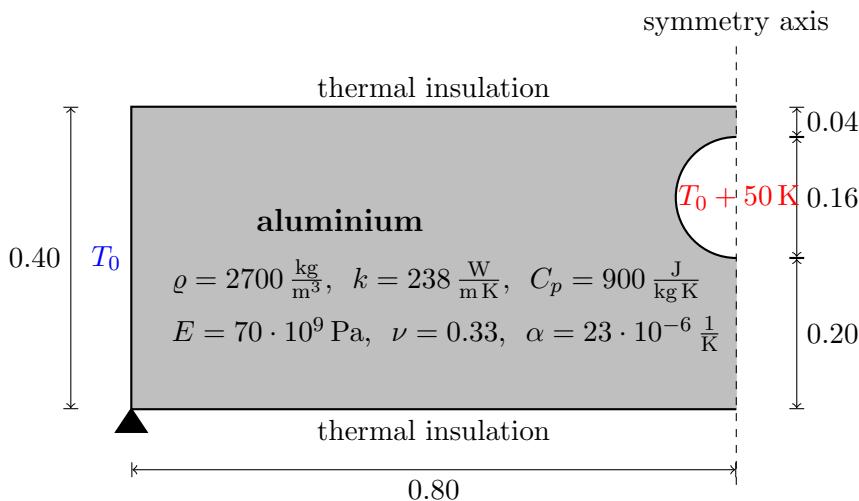


FIGURE 1: An uncoupled theromelastic problem: solve the conductive heat transfer problem and use the temperature variation obtained in the domain as a thermal load for a coupled mechanical problem.

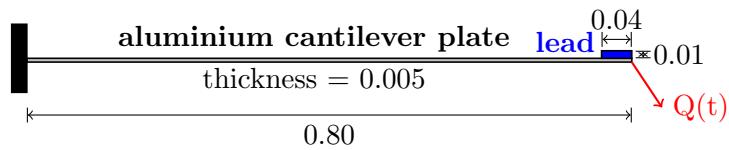
Exercise 4.3

Using the Weak Form PDE Interface in COMSOL Multiphysics

Weak form for harmonic linear elasticity

$$\omega^2 \int_{\Omega} \varrho u_i \delta u_i - \int_{\Omega} \sigma_{ij} \delta u_{i|j} + \int_{\Omega} f_i \delta u_i + \int_{\Gamma_t} \hat{t}_i \delta u_i = 0$$

Here: $\sigma_{ij} = \sigma_{ij}(\mathbf{u}) = \begin{cases} C_{ijkl} u_{k|l} & \text{-- for anisotropic material} \\ \mu (u_{i|j} + u_{j|i}) + \lambda u_{k|k} \delta_{ij} & \text{-- for isotropic material} \end{cases}$



$$\rho_{Al} = 2700 \frac{kg}{m^3},$$

$$E_{Al} = 70 \cdot 10^9 Pa,$$

$$\nu_{Al} = 0.33,$$

$$\rho_{Pb} = 11340 \frac{kg}{m^3},$$

$$E_{Pb} = 16 \cdot 10^9 Pa,$$

$$\nu_{Pb} = 0.44.$$

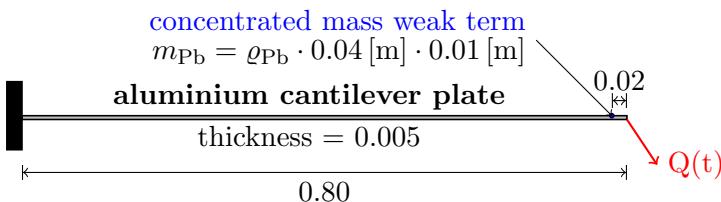


FIGURE 2: Simplified simulation of the influence of a heavy lead lump by adding a concentrated mass term to the weak form of a harmonic elastodynamic problem.

- Constants:

```
omega = 2*pi*f
mu = E/2/(1+nu)      lam = nu*E/(1+nu)/(1-2*nu)
```

- Domain expressions (for an isotropic material):

```
s11 = 2*mu*u1x + lam*(u1x+u2y)
s22 = 2*mu*u2y + lam*(u1x+u2y)
s12 = mu*(u1y+u2x)
```

- Domain integrand (in Ω):

```
omega^2*rho*( u1*test(u1) + u2*test(u2) )
- s11*test(u1x) - s12*test(u1y+u2x) - s22*test(u2y)
f1*test(u1) + f2*test(u2)
```

- Neumann boundary integrand (on Γ_t):

```
t1*test(u1) + t2*test(u2)
```

- Concentrated mass weak term:

```
omega^2*mass*( u1*test(u1) + u2*test(u2) )
```